

# A FULL ALTERNATIVE FOR THE RTD QUANTUM-INDUCTANCE EQUIVALENT-CIRCUIT MODEL

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## ABSTRACT

Under specific conditions, the small-signal series/parallel double-RC equivalent-network is a novel full mutual alternative for the resonant tunnelling diode quantum-inductance circuit model. Network optimisations to accurately match measured intrinsic impedances of stable, non-oscillating GaAs/AlAs devices, pointed at these conditions. The capacitance  $C_w$  of the series-RC branch, peaks needle-sharp at the negative dynamic conductance maximum, indicating carrier discharge from the quantum well. The  $R_b C_w$ -time constant equals  $L_q G_d$  of the quantum-inductance model, so it is also an indication of the quasibound-state lifetime in the well. For CAD purposes, a very good RTD intrinsic impedance description in the entire bias/frequency space (0-2 V; 0.05-40.05 GHz) is obtained with frequency-independent intrinsic elements, scalable with device area.

## INTRODUCTION

Several equivalent circuits for small-signal impedance modelling of double barrier resonant tunnelling diodes (RTDs) are available from literature. We recently studied the application of the RCL or quantum-inductance (QI) model (Fig. 1a; Brown et al [1], Vanbesien et al [2], Kwaspen et al [4,5]). Another model, previously published by researchers from Leeds and Nottingham Universities, U.K. (Miles et al [3]), also can be used to describe measured microwave impedances of GaAs/AlAs based RTDs with symmetric thin barrier and spacer layers. Preliminary optimisations of this series/parallel double-RC network (henceforth indicated as SPdRC; Fig. 1b) to fit the measured data, showed that the  $R_b C_w$ -time constant of the series-branch behaved almost similar as the  $L_q/R_d$ -time constant of the QI-model. A

mathematical impedance analysis of both models shows that, under specific conditions, the SPdRC equivalent network is a full alternative for the QI-model. While the last has four frequency-independent intrinsic elements to describe the measured impedance 'perfectly', the SPdRC-network has one degree of freedom more. The specific conditions reduce the redundancy and a novel full mutual alternative is obtained. Repeated optimisations with these conditions set, resulted in a very good description of the measured intrinsic RTD-impedances throughout the whole 0-2 V bias-voltage and 0.05-40.05 GHz frequency ranges.

## MODEL DESCRIPTIONS AND EQUIVALENCE-CONDITIONS

The small-signal dynamic device resistance  $R_d$  ( $R_D$ ) (Fig. 1), should agree the differential resistance derived from the DC I-V curve of the stable RTD.  $C_d$  ( $C_D$ ) is the dynamic device capacitance. The authors of the SPdRC-model [3], denoted  $C_w$  to represent the charge in the well while  $R_b$  is the resistance of the barrier closest to the cathode.  $R_s$  describes contact and spreading resistances and  $L_q$  is the intrinsic quantum inductance. The impedances  $Z_{QI}$  and  $Z_{SPdRC}$  of both intrinsic RTD models are in a certain stage of the analysis:

$$Z_{QI} = (R_d + j\omega L_q) / ((1 - \omega^2 C_d L_q) + j\omega R_d C_d) + R_s \quad (1)$$

$$Z_{SPdRC} = (R_D + j\omega R_b R_D C_w) / ((1 - \omega^2 R_b R_D C_D C_w) + j\omega (R_D C_D + R_b C_w + R_D C_w)) + R_s \quad (2)$$

Intended to describe the same intrinsic RTD, comparison of the model impedances, term by term, leads to :

$$R_d = R_D, \quad L_q = R_b R_D C_w \quad \text{and} \quad C_d L_q = R_b R_D C_D C_w \quad \text{which gives} \quad C_d = C_D, \quad \text{and} \\ R_d C_d = R_D C_D + R_D C_w + R_b C_w \quad (3)$$

When the condition  $R_b = -R_D$  ( $= -R_d$ ) is set in the SPdRC-model,  $R_D C_w + R_b C_w$  of equation 3 cancel out, and a full mutual alternative is obtained ( $Z_{QI} = Z_{SPdRC} = Z_d$ ). One model can be expressed into the other one. Then the time constant  $L_q/R_d = L_q G_d$  can be written as  $R_b C_w$ .

## MEASUREMENTS AND OPTIMISATION RESULTS

The RTD under test, is a 6  $\mu\text{m}$  square device with a 5 nm GaAs quantum well and symmetric 2.5 nm thick AlAs barriers and GaAs spacer layers, all undoped, plus upper and lower contact layers on a semi-insulating substrate (Fig.2).

A microwave reflection coefficient array  $S_{11}[V_b, f]$ , on-wafer measured on this RTD under stable, non-oscillating conditions, was used as input for an optimisation process that matches the SPdRC circuit response to the measured data. The  $S_{11}$  datasets (bias range 0-2 V, 75 points; frequency range 0.05-40.05 GHz, 401 points) of the extrinsic RTD were converted to a measured impedance array  $Z_d[V_b, f]$  of the intrinsic RTD, by using measured data of reference structures that describe the behaviour of the interconnections on the substrate, from the  $S_{11}$

measurement plane to the RTD-mesa (Fig. 3; [4]). The measured and modelled real and imaginary parts of  $Z_d$  are compared and the model is optimised (for each bias point) for minimum absolute errors. The  $R_b = -R_D$  condition is set during the optimisations. Fig. 4 shows an example of a match at 1.0090 V bias in the active region. In this way, all 75 bias points are treated and the optimised model elements are assembled to give Fig. 5b-c.  $R_s$  has an average value of 9.5  $\Omega$ . Fig 5a shows the measured DC I-V curve of the stable, non-oscillating RTD at 21°C [4]. Fig 5d gives the measured and modelled resistive cut-off frequency  $f_r$  against bias voltage (See also Fig. 4a ). From the optimised independent elements, the time constants  $R_b C_w = L_q G_d$  (peak ~22ps at 1.0008-1.0124 V) and  $R_d C_d$  are calculated (Fig. 6a,b). Note that the extreme values of  $R_b C_w$  at the peak and valley voltages are less reliable, since  $G_d$  ( $G_b$ ) goes through zero there.

## DISCUSSION

In contrast to the conclusion about the  $C_w$ -peak location in [3], the network optimisations on our RTD, set the onset of  $C_w$  at the current maximum, while  $C_w$  and  $G_d$  peak at the same bias, so  $C_w$  indicates only charge transfer out of the quantum well. The distorted I-V curve in [3], due to relaxation oscillations, probably led to the faulty statement.  $C_d$  behaves generally as a depletion capacitance. Because  $G_b$  and  $G_d$  are reversed by the equivalence condition set,  $G_b$  and  $C_w$  are negative in the passive regions to give a positive  $L_q$ . However, the influence of the series-branch in these regions is very limited, since, from optimisations,  $C_w$  is very small, because the Esaki-subcircuit ( $R_d$ ,  $C_d$  and  $R_s$ ) is sufficient for a good fit of measured and modelled  $Z_d$  in the passive regions. The time constant  $L_q G_d = R_b C_w$  should be an indication of the quasibound-state lifetime in the well [1,2]. The calculated ground-state lifetime for a barrier thickness of 2.55 nm is ~ 50 ps and changes exponentially to ~ 18 ps for 2.26 nm thickness (1 monolayer decrease). This compares well with a time constant of 22 ps measured at 1.0072 V (Fig. 6a). The  $f_r$ -curves match very well, an indication of a good model fit, so this paper reflects also a plea for impedance measurements on stable, non-oscillating RTDs when extracting model parameters.

For CAD purposes, a very good RTD intrinsic impedance description in the entire bias/frequency space (0-2 V; 0.05-40.05 GHz) is obtained with frequency-independent intrinsic elements, scalable with device area.

## ACKNOWLEDGMENTS

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\*\* Mr van der Vleuten passed away in May of this year.

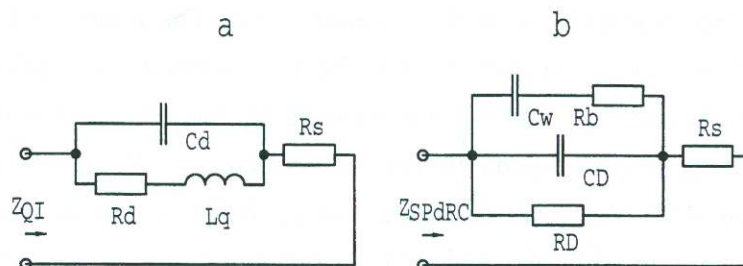


Fig. 1 Intrinsic RTD equivalent-circuits  
 a Quantum-inductance model  
 b Series/parallel double-RC network

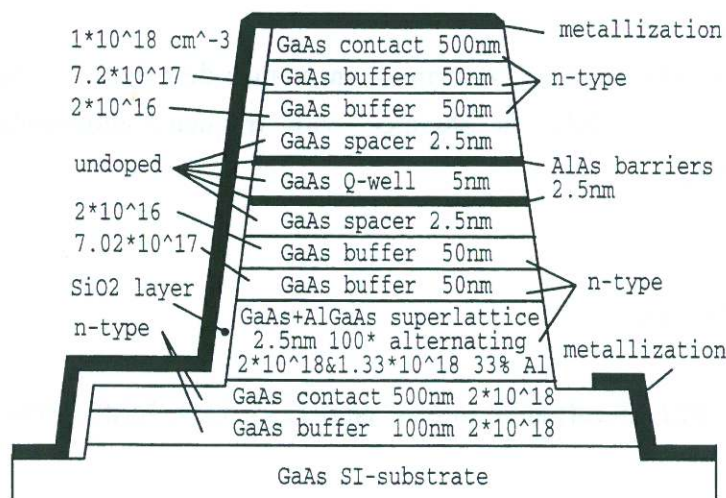


Fig. 2 RTD layer structure

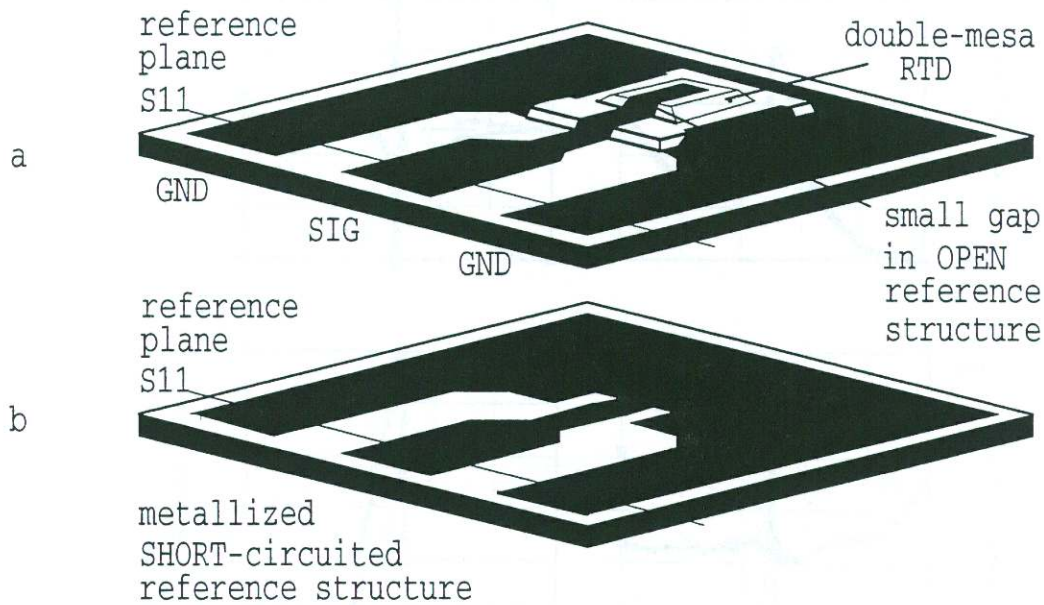


Fig. 3 Planar RTD with coplanar microwave probe access and metallized reference structures SHORT and OPEN  
 a planar RTD with double-mesa structure  
 b short-circuited reference structure to determine the elements of the extrinsic model

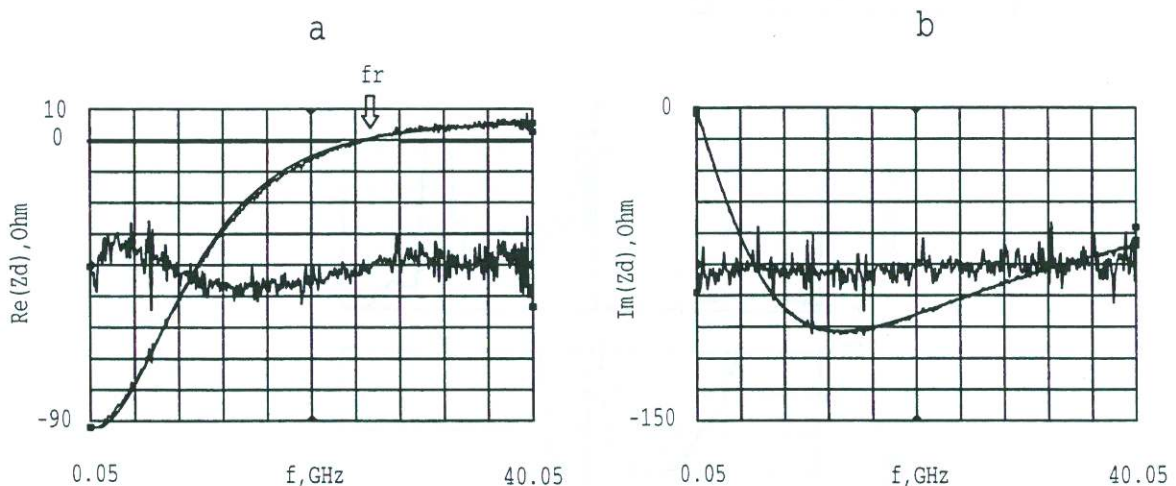


Fig. 4 Measured and modelled intrinsic impedance  $Z_d$  of RTD @ 1.009 V ; Noisy curve is difference measured-modelled (2 Ohm/div; center= 0)  
 a real part of  $Z_d$  against frequency  $f$  (GHz)  
 b imaginary part of  $Z_d$  against frequency

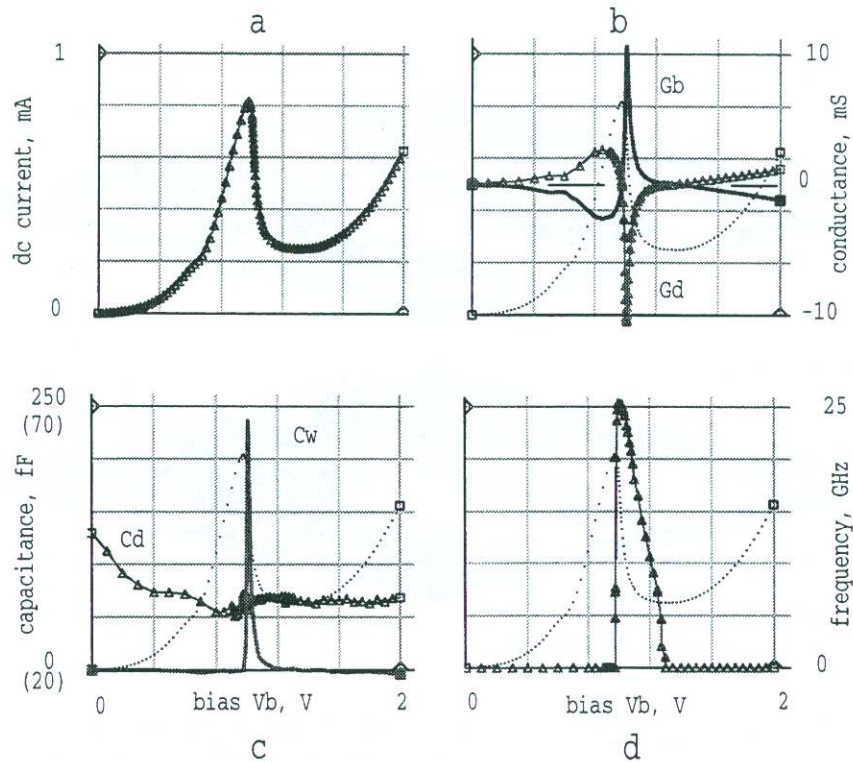


Fig. 5 Results measurements and optimisations  
 a measured DC I-V curve; also dotted lines in Fig. 5b-d  
 b dynamic conductances  $G_b$ ,  $G_d$  [mS] against bias-voltage  $V_b$   
 c dynamic capacitances  $C_d$  and  $C_w$  against  $V_b$ .  
 ranges are 20-70 fF ( $C_d$ ) and 0-250 fF ( $C_w$ )  
 d measured (-) and modelled ( $\Delta$ ) resistive cutoff  
 frequency  $f_r$  in GHz

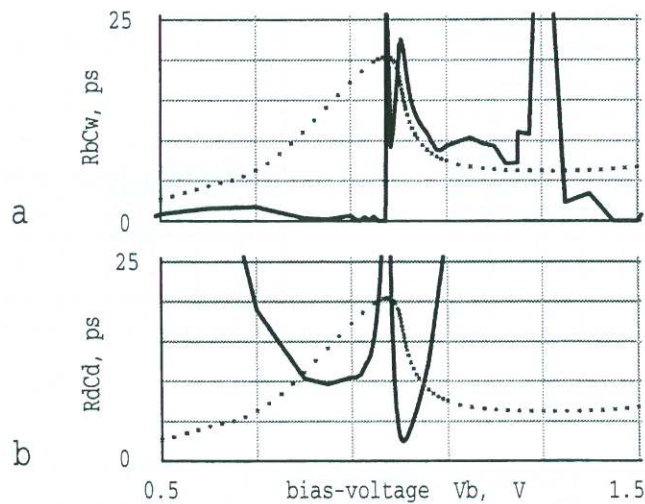


Fig. 6 Time-constants  $R_b C_w$  and  $R_d C_d$   
 Dotted line is DC current (1 mA f.s.)  
 a  $R_b C_w$  ( $= L_q G_d$ ; in ps) against bias  $V_b$   
 b  $|R_d|.C_d$  ( $= |R_b|.C_d$ ; in ps)